

TITLE: FOURTH QUARTERLY REPORT OF STUDY OF CAPACITORS
FOR STATIC INVERTERS AND CONVERTERS

(MAY 16, 1964 - AUGUST 16, 1964)

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PREPARED FOR THE

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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By J. F. Scoville

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TECHNICAL MANAGEMENT
NASA-LEWIS RESEARCH CENTER
AUXILIARY POWER GENERATION OFFICE
FRANCIS GOURASH

PREPARED FOR THE

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

By J. F. Scoville



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SUMMARY

This is the fourth quarterly report for the "Study of Capacitors for Static Inverters and Converters".

The objectives of the study are to establish capacitor AC characteristics and ratings for reliable operation in aerospace static inverter and converter applications and to facilitate minimum capacitor Volume and Weight selection consistent with maximum equipment performance and reliability.

This study was initiated to obtain capacitor AC data and characteristics that are considered essential in the selection of static inverter and converter capacitors for space applications.

General Electric's Specialty Control Department in Waynesboro, Virginia is conducting this study.

This report covers the work accomplished from May 16, 1964 through August 16, 1964 and contains:

- a) Capacitor dissipation factor and capacitance versus temperature and frequency.
- b) Comparison of metallized paper polycarbonate-foil, and metallized polycarbonate capacitor dissipation factors.
- c) Results of a 1000 hour capacitor life test with 400 cps voltage and 85°C ambient.

INTRODUCTION

Capacitors being evaluated in this study are limited to those suitable for use in aerospace static inverters and converters operating in space environments. Inverter rating guides used in this capacitor study are 115/200 volt, 3-phase, 400 cps, 0.1 to 10.0 kilowatt output with input voltage range from 25 to 105 volts D.C.

The need for this study was influenced by the stringent requirements imposed on capacitors by the operating nature of equipment in space environment and by the general lack of capacitor AC characteristics and data.

Heat is generated within commutating and filter capacitors because the voltampere-dissipation factor products are appreciable. In commutating capacitors,
the volt-ampere product is less than in filter capacitors, but the commutating
pulse and ripple frequencies have larger dissipation factors than at the
filter capacitor frequency. Transfer of the heat losses within the capacitors
are usually limited to conduction across their mounting surfaces to radiator
cooling systems on spacecraft. Lack of adequate capacitor AC data and
characteristics could result in weight and reliability penalty factors in
aerospace static inverter and converter applications.

Objectives of this study are to obtain capacitor AC data and characteristics to facilitate proper capacitor selection for aerospace static inverter and converter applications.

There are four (4) phases in this study: (1) Defining Capacitor State-of-the-Art Survey; (2) Conducting Capacitor State-of-the-Art Survey; (3) Experimental Testing of Capacitors; and (4) Capacitor Evaluation and Recommendations.

During the first three quarterly report periods, the Capacitor State-of-the-Art Survey was defined and conducted. Sample quantities of metallized polycarbonate, polycarbonate/foil and metallized paper capacitors were procured for experimental testing. Results of the survey revealed that polycarbonate dielectric capacitors are considered state-of-the-art capacitors. Metallized polycarbonate capacitors approach metallized paper capacitors in price, weight and volume, but the lower dissipation factors may result in significant weight and volume advantages in certain AC applications. Analysis of commutating capacitor losses, reported in the 3rd. Quarterly Report, illustrated that capacitor losses, while subjected to complex waveforms, may be predicted from capacitor characteristics determined from sinusoidal waveforms.

This is the fourth quarterly report for the work accomplished between May 16, 1964, and August 16, 1964. During this period the experimental testing was in progress. Test results included in this report are capacitance and power factor values versus temperature and frequency and results of 1000 hour capacitor life test at 85°C with 400 cps voltage.

1.0 Capacitance and Disspation Factor Tests

1.1 Purpose

Capacitance and dissipation factor values for polycarbonate and paper capacitors from several manufacturers are being determined by test over a temperature range from = 55°C to + 85°C and frequency range from 400 cps to 10 kilocycles. In addition dissipation factors for a few capacitors are being obtained at frequencies up to 60 and 80 kilocycles. These data will provide equipment designers and capacitor manufacturers with characteristics that will facilitate proper selection of capacitors for aerospace inverter and converter applications. Laboratory temperature and frequency test data are available for dielectric films, but capacitors contain materials other than the dielectric films and require construction techniques which can alter the capacitor characteristics. These construction techniques include mounting of the capacitor roll or stack within the container, end connections to the capacitor and impregnants or fillers if any are used.

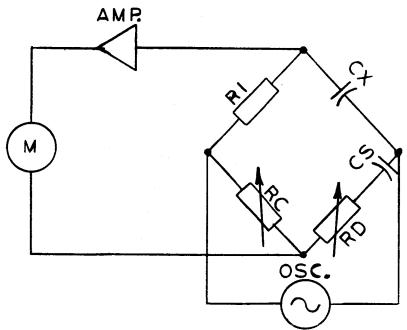
1.2 Description of Tests

Capacitance values were determined with an impedance bridge constructed for these tests. This bridge was constructed with components and interconnections that resulted in a minimum of reactance and therefore little error was introduced by the bridge over the frequency range. An elementary diagram of this type bridge is shown in Figure 1. Capacitance values measured with this bridge compared favorably with values obtained with a General Radio Model 716-C and Sprague Model IW2 capacitance bridges.

Capacitor dissipation factors obtained from the impedance bridge measurements provide comparative data that was adjusted by correction factors obtained from calorimeter heat loss measurements. Adjustment of these dissipation factor data is necessary because unknown and stray capacitances can be appreciable in the range of interest.

Use of the calorimeter is made in measuring the rate of heat being generated from a capacitor immersed in a fluid by observing the rate of temperature rise. Calibration of the calorimeter is accomplished by mounting known values of resistors to the capacitor surface within the calorimeter and measure the direct current flowing in the resistor while observing the rate of temperature rise of the calorimeter fluid. Caution was exercised to obtain the rate of temperature rise after the thermal inertia had been overcome.

Elementary Diagram of Impedance Bridge



RI= 99.7 OHMS; CS=.OIMFD., GEN.RADIO STD. 1409L

CX = Capacitor under test

RC= Adjustable resistance (switch, fixed resistors and a potentiometer)

RD= Adjustable resistance (switch, fixed resistor and a potentiometer)

AMP - Battery operated, single stage, transistor amplifier

M - Harmonic Wave Analyser - used as null detector

Where R_{CX} is the effective resistance of capacitor under test.

Capacitance:
$$\frac{R1}{RC} = \frac{I_{CX}}{I_{CS}}$$
 $CX = \frac{CS(RC)}{RI}$

Photographs of the calorimeter, test equipment and calorimeter test specimen mounting were shown in the 3rd. Quarterly Report and are shown in Figures 2 and 3 of this report for convenience to the reader. A calorimeter calibration curve is also repeated for the reader in Figure Cl.

Calculation of the rate of heat input is obtained from:

I²R = Watts = °C/mimute calorimeter fluid

Calculation of the capacitor dissipation factor is calculated from:

D.F. = Watts where Watts = Rate of temperature rise Calibration rate of temperature rise

Care was exercised to minimize the calorimeter heat loss rate by maintaining the calorimeter fluid temperature within $+2^{\circ}$ C of the calorimeter external ambient ($2h - 26^{\circ}$ C within the enclosure). Maintaining the calorimeter fluid within $+2^{\circ}$ C of the ambient temperature was accomplished by replacement of the fluid between tests.

Impedance bridge measurements at 25°C ambient and up to 10 kilo-cycles have been made for eighty-five (85) capacitors and correction factors to adjust the bridged dissipation factor values for fifty-five (55) capacitors have been applied.

Capacitance and dissipation factors of seventeen (17) capacitors were measured by the impedance bridge over the temperature range up to 10 kilocycles. Correction factors for eleven (11) of these capacitors have been obtained.

1.3 Results of Tests in 25°C Ambient

Impedance bridge capacitor test data over a frequency range from 0.4 to 10 kilocycles in 25°C ambient with simusoidal voltage wave-form for fifty-five (55) capacitors are tabulated in Tables A-1 through A-3 in Appendix A.

1.3.1 Metallized Polycarbonate Capacitors

Table A-1 contains capacitance and percent dissipation factor test data for twenty-five (25) metallized polycarbonate capacitors.

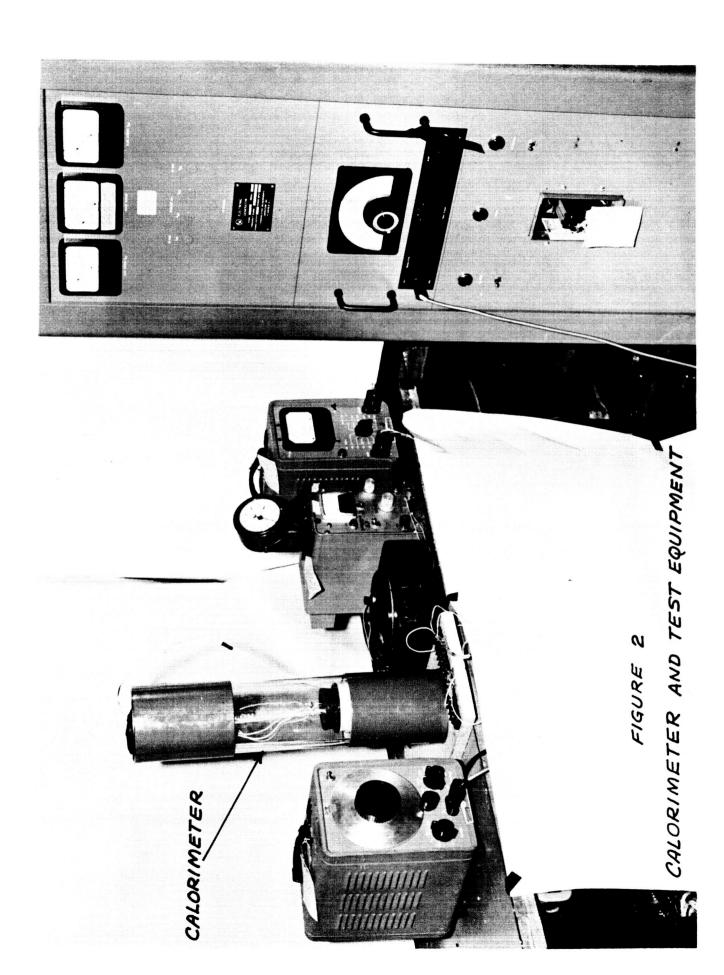




FIGURE 3

TEST SPECIMEN MOUNTING IN CALORIMETER

Capacitor dissipation factor used in this report is defined as the ratio of the resistive component to the capacitive reactance component. The capacitors used in this study have very large capacitive reactance components compared to the resistive components and resulting errors are small as shown below:

$$\frac{Rc}{j\lambda c} = \frac{Rc}{Rc + j\lambda c} \quad \text{where } Rc \ll \lambda c$$

The curve in Figure Al illustrates 8.2 percent capacitance variation and 2.7 percent average capacitance variation versus frequency for the capacitors tabulated in Table A-1.

With the exception of capacitors 2B, 2E, 3A through 3E listed in Table Al, the percent dissipation factor (D.F.%) versus frequency for the remaining eighteen (18) capacitors is shown in Figure A2. The variation ranges from 0.092 to 1.020 percent. Capacitor numbers that were excluded from the data presentation in Figure A2 were considered to have excessively high dissipation factor percentages by comparison with the remaining eighteen (18).

Manufacturers of the seven (7) capacitors with the high dissipation factors are being advised of these test results and effort will be made to determine the cause for the high dissipation factors.

1.3.2 Polycarbonate/Foil Capacitors

Table A-2 contains capacitance and percent dissipation factor test data for fifteen (15) polycarbonate/foil capacitors.

The composite curve in Figure A3 illustrates 10.5 percent capacitance variation versus frequency and average capacitance variation of 2.8 percent for the capacitors tabulated in Table A-2.

Dissipation factor variation from 0.05 to 0.2h percent versus frequency is shown in Figure Ah for the capacitors tabulated in Table A-2.

Figure 6 contains the percent dissipation factor up to 50 and 80 kilocycles for capacitor numbers 9B, 10A, and 11A. Capacitor number 10A has the highest dissipation factor of 2.64 percent at 60 kilocycles. Dissipation factor data for a 2 MFD, 400 VDC metallized paper capacitor is also plotted in Figure 6 for reference purposes.

1.3.3 Metallized Paper Capacitors

Capacitance and percent dissipation factor test data for fifteen (15) metallized paper capacitors are tabulated in Table A-3.

Figure A5 illustrates a capacitance variation versus frequency of 3.7 percent and an average capacitance variation of 1.3 percent for the capacitors tabulated in Table A-3.

Dissipation factor variation versus frequency from 0.19 to 1.54 percent for the capacitors tabulated in Table A-3 is shown in Figure A6.

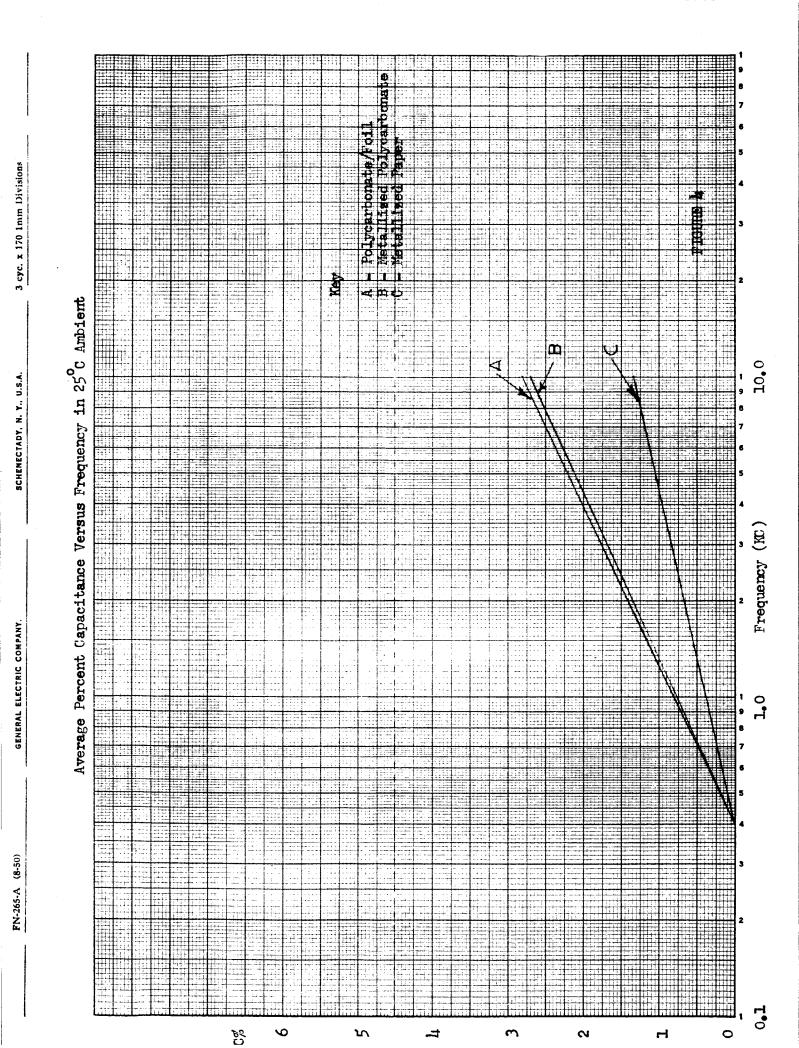
1.3.4 Comparison of Capacitor Types

Comparison of the average data plotted in Figures 1A, 2A, 3A, 4A, 5A and 6A are presented for convenience to the reader in Figures 4 and 5. From these graphs, one may observe that the dissipation factor for polycarbonate/foil capacitors is approximately one quarter (1/4) as large as that for metallized paper capacitors. Also the dissipation factor for metallized polycarbonate capacitors is approximately two-thirds (2/3) that of metallized paper capacitors.

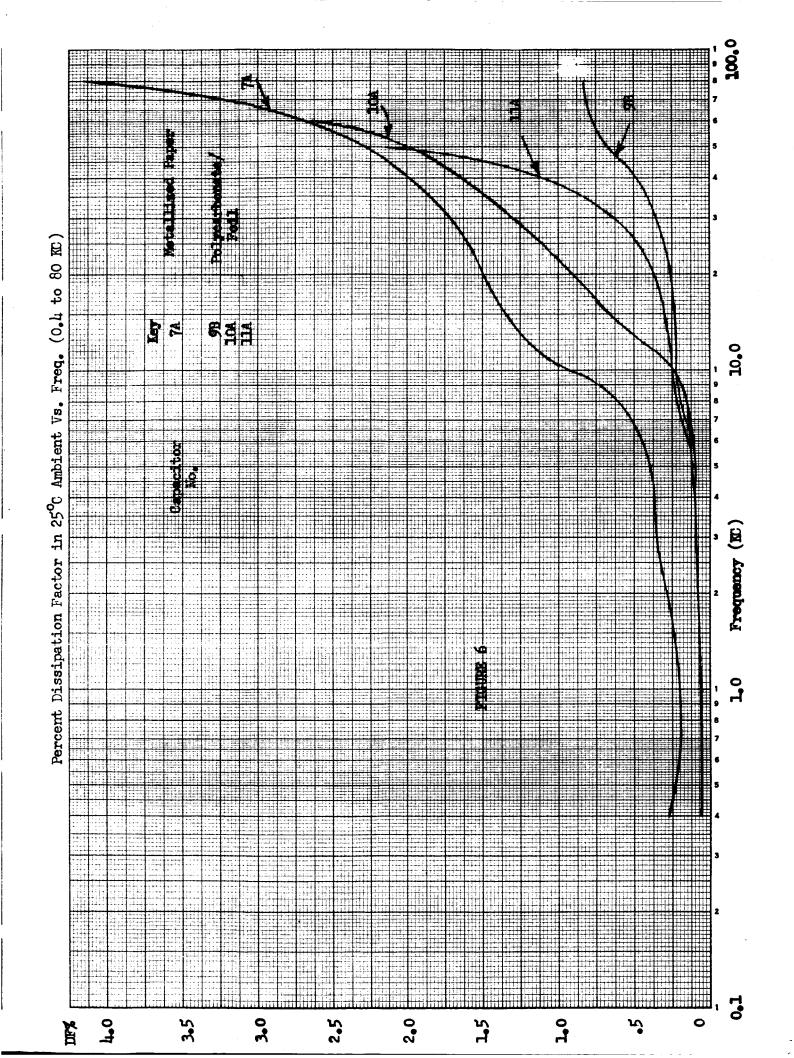
Variation of the average percent capacitance variation is less than 1.6 percent between the three (3) types of capacitors.

The dissipation factor for polycarbonate film is considerably smaller than for paper dielectrics used in capacitors. However, part of this material advantage may not be realized if capacitor end connections and conductive elements contribute resistive losses approaching the same order of magnitude as the dielectric material.

The difference in dissipation factors between metallized paper and metallized polycarbonate capacitors would appear to be attributed largely to the dielectric material advantage of polycarbonate. The difference in dissipation factors between metallized polycarbonate and polycarbonate/foil capacitors appear to be attributed to capacitor end connections and less resistance in the thicker foil, as the capacitor conductive element, than the thinner metallized conductive element.



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Although metallized paper capacitors have larger dissipation factors than polycarbonate capacitors, they exhibit smaller percent capacitance change versus frequency in 25°C ambient. This smaller percent change of capacitance is believed to be attributed to a slightly decreasing capacitance characteristic with increasing frequency for impregnated paper dielectrics if it is assumed that the series inductive elements from construction methods in the paper and polycarbonate capacitors are identical.

1.4 Results of Tests Versus Temperature and Frequency

Impedance bridge capacitor test data in ambient temperatures from 55°C to + 85°C over a frequency range of 0.4 to 10 kilocycles with simusoidal voltage waveform for eleven (11) capacitors are tabulated in Tables A-4 through A-6 in Appendix A.

1.4.1 Metallised Polycarbonate Capacitors

Table A-4 contains capacitance and dissipation factor test data for five (5) metallized polycarbonate capacitors. A variation of -2.0 to +1.6 percent capacitance referenced to 25°C values versus frequency and temperature, for the capacitors listed in Table A-4, is shown in Figure A7. With the exception of capacitor numbers 2E and 3D, a variation from 0.09 to 1.23 percent dissipation factor versus frequency and temperature is shown in Figure A8 for the remaining capacitors listed in Table A-4. Exclusion of the dissipation factor data for capacitor number 2E from Figure A8 was done because the dissipation factor percent in -55°C ambient was considered to be abnormally high and a function of either construction techniques or material other than metallized polycarbonate film. Similarly, data for capacitor number 3D was excluded from Figure A8, because the high dissipation factor may be a function of construction techniques.

1.4.2 Polycarbonate/Foil Capacitors

Capacitance and dissipation factor test data for three (3) polycarbonate/foil capacitors are tabulated in Table A-5.

Variation of -2.1 to +0.65 percent capacitance for the three (3) capacitors listed in Table A-5 is illustrated in Figure A9. With the exclusion of dissipation factor test data for capacitor number 10A, a variation from 0.03 to 0.275 percent dissipation factor for the other two (2) capacitors in Table A-5 is illustrated in Figure Alo. Exclusion of the dissipation factor data for

capacitor number 10A from Figure AlO was done because of the relatively high percent dissipation factor in - 55°C ambient that may be a function of construction technique or material other than the dielectric.

1.4.3 Metallized Paper Capacitors

Capacitance and dissipation factor test data for three (3) metallized paper capacitors are tabulated in Table A-6.

Percent capacitance variation from - 13.75 to + 3.0 percent referenced to 25°C values for the capacitors listed in Table A-6 is illustrated in Figure All. Percent dissipation factor variation from 0.175 to 1.44 percent for the capacitors listed in Table A-6, with the exception of capacitor number 8A, is illustrated in Figure Al2. Exclusion of the percent dissipation factor data for capacitor number 8A from Figure Al2 was for the same reason for the exclusion of data for capacitor number 10A in paragraph 1.4.2 above.

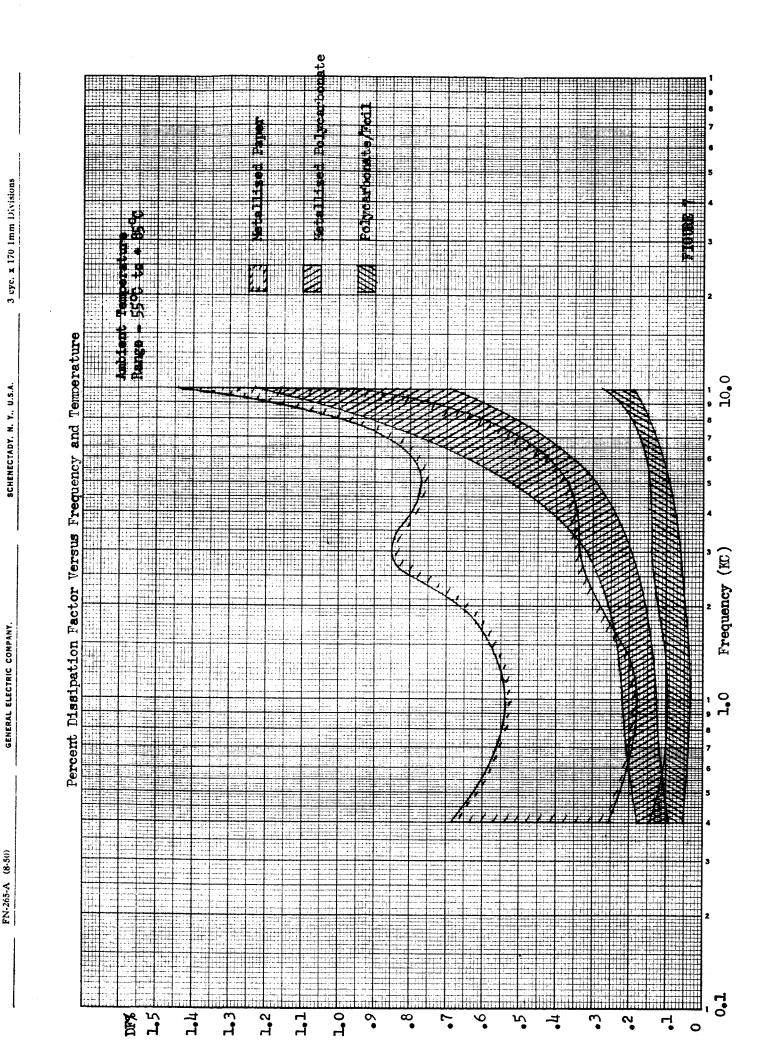
1.4.4 Comparison of Capacitor Types

Comparison of the dissipation factor data plotted in Figures A8 through A12 are presented in Figure 7 to illustrate the differences of the three (3) types of capacitors tested in this study. In comparison with metallized paper capacitors, polycarbonate/foil capacitors have dissipation factors of approximately one-fourth (1/4) and metallized polycarbonate capacitors have values approximately one half (1/2) to two-thirds (2/3).

The capacitor dissipation factor data in Figure 7 are based on:

- A) Polycarbonate/foil Three capacitors from 2 manufacturers
- B) Metallized Polycarbonate Two capacitors from 2 manufacturers
- C) Metallized Paper Two capacitors from 1 manufacturer

These capacitor dissipation characteristics plotted in Figure 7 are considered to be typical for the capacitor types indicated because 25°C ambient data for a larger number of similar capacitors listed in Tables Al through A3 exhibit relatively small variation of dissipation factors between manufacturers except those capacitors previously mentioned in paragraphs 1.4.1. 1.4.2 and 1.4.3 above.



A tabulation of the tubular capacitor sizes and weights by type is presented in Table I. In the 400 VDC ratings, the ratio of the average volume/capacitance of metallized polycarbonate to metallized paper capacitors is 116 percent and similarly the ratio for the 200 VDC ratings is 138 percent. This 22 percent increase in volume/capacitance ratio from the 400 VDC to the 200 VDC ratings may be attributed to a minimum polycarbonate film thickness limitation.

The volume/capacitance ratio between polycarbonate/foil and metallized paper capacitors is 250 percent for the 400 VDC ratings and 450 percent for the 200 VDC ratings. From these large ratios, it appears that the foil thickness may approach the polycarbonate film thickness.

The pounds/capacitance for metallized polycarbonate is approximately the same as for metallized paper capacitors. Larger physical size of the polycarbonate capacitors, compared with metallized paper, account for the larger pounds/capacitance figure.

2.0 Capacitor Life Test

2.1 Purpose

A total of fifty (50) capacitors were subjected to an abbreviated life test of 1000 hours in 85°C ambient. This test was conducted to determine if the capacitors could withstand AC peak voltages equivalent to the DC voltage ratings with the exception of DC voltage ratings above corona starting voltage region.

2.2 Description of Test

The fifty (50) capacitors (33 metallized polycarbonate, 12 polycarbonate/foil and 5 metallized paper capacitors) were mounted on the inner walls of a sealed aluminum box, shown in Figure 8. The surface of the aluminum box was maintained at a temperature of 85 + 3°C for the duration of the life test. Figure 9 shows the indicating lights that are in parallel with the fuses in each capacitor circuit illustrated in the elementary diagram in Figure Bl in Appendix B.

The rating of the fuses in series with the capacitors were selected to be approximately three (3) times the rated capacitor current. Detection of a shorted capacitor during the test was revealed by the indicator light that was on, indicating the fuse had open circuited.

Tabulation of Secardior Publicar Signs and Weights

Capacitor Identification	To see all of	.35			Average	
No.	LOTE	300 Mg	Type	in3/cF	Vol./uF/Type	#/uF
1A-1E 2A-2E 3A-3E 5A-5E	1 @ 2 uf 2,5 uf 2 uf		MFC MFC MFC	0,91 0,94 1,03 ,34	0,93	.063 .062 .059 .053
7A-7E 8A-8E	2 uF 2 uF		MP MP	.89 .71	0,80	.064 .052
9A-9E			PCF	2.06	2,06	.145
12A - 12E 13A-13E 14A-14E 15A-15E		3 W 3 W 3 W 3 W	MFC MFC MFC MFC	0,35 0,28 0,56* 0,24	0,29	.023 .018 .036 .017
14A_4E 16A_16E		2 uF 3 uF	MP MP	0,22 0,21	0,21	.018
10A-10E		2 uF	PCF	0,93	0,93	•069

MPC - Metallised Polycarbonate
Key: MP - Metallised Paper
PCF - Polycarbonate/Foil

* Omitted in the Average Vol/uF/Type figure

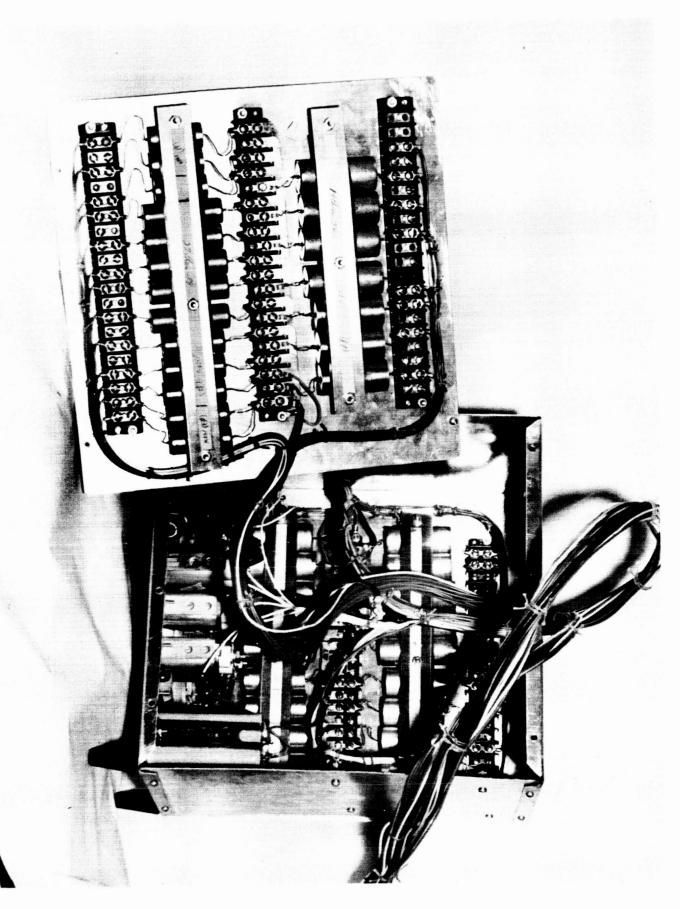


FIGURE 8 Mounting of Life Test Capacitors

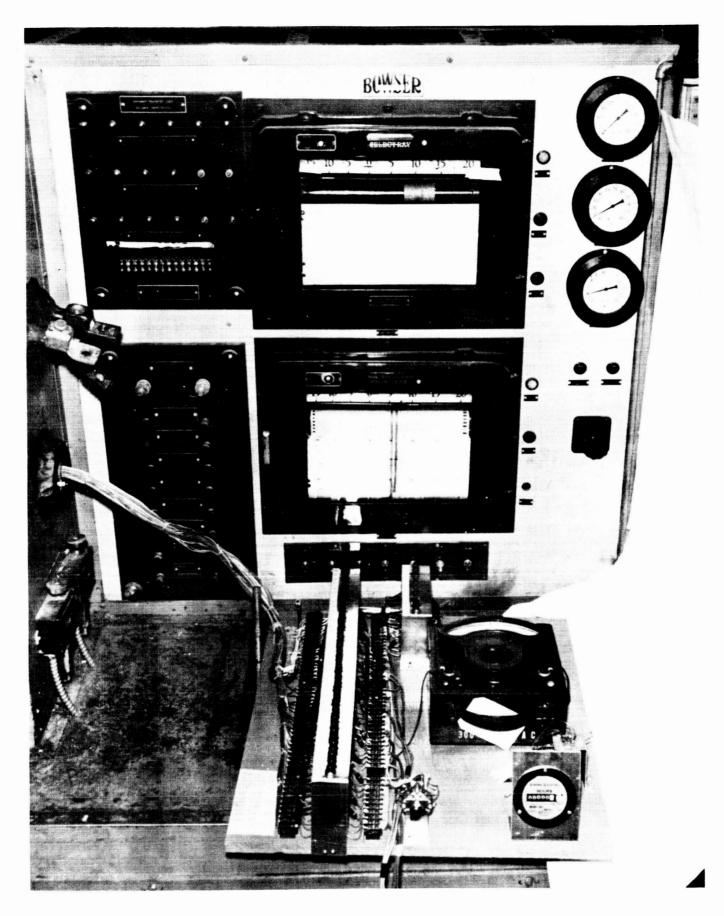


FIGURE 9 Life Test Monitoring Equipment

Capacitors that may have failed in an open circuit mode only would have been detected when capacitance and dissipation factor data were taken at the conclusion of the test.

All capacitors were energized with 420 cps voltage with peak voltage comparable to the capacitor DC voltage rating with the exception of the 400 VDC ratings which were energized with 325 volt peak. The 325 peak voltage is approaching the corona start region.

A strip chart temperature recorder shown in Figure 9, was used to monitor the temperature of the aluminum box containing the capacitors. The 420 cps voltage was monitored twice during each normal working day during the test. An elapsed time indicator was energized from the 420 cps voltage source to indicate total test time.

2.3 Results of Test

There were thirteen (13) capacitors that failed during the life test. The types that failed by developing short circuits were:

Q'ty	Туре	Rating
3 3	Polymarbenate/foil Polymarbenate/foil	l med, loo ydd 2 med, 200 ydd
	Metallized Polycarbonate	2 MFD, 400 VDC 3 MFD, 200 VDC

Capacitors 3, h_2 5, 11 in Figure 12 developed short circuits upon step application of the 230 volt RMS, h20 cps power. This step application of power resulted in two (2) 350 V RMS transients and three (3) 280 V RMS transients from resonant effects between the capacitors and the transformer inductance.

Capacitors 20, 21, 23 and 30 in Figure 1B developed short circuits upon application of power.

The following capacitors developed short circuit during the life test as tabulated:

Capacitor No.	Hours to Failure
13 32	234.7 362.7
12, 33	362.7 474.8 666.7
31.	666 _• 7

The capacitors that failed during this test were from one (1) capacitor manufacturer. The fifty (50) capacitors subjected to this life test were obtained from six (6) capacitor manufacturers. Capacitors that developed short circuits during this life test are being returned to the capacitor manufacturer for determination for cause of failure.

3.0 Work Planned for the Next Report Period

Completion of this study has been rescheduled from August 16, 1964 to October 16, 1964 to permit analysis and reporting of reasons for large dissipation factor variation versus frequency and temperature, determination of causes for capacitor failure in life test and to complete calorimeter testing of larger 3 and 5 microfarad capacitors to obtain correction factors for bridge data.

4.0 Conclusions

Reduction of commutating capacitor heating will be achieved if the equipment designer can reduce or eliminate high frequencies from being impressed on the capacitor because the dissipation factor increases rapidly with frequency above 10 kilocycles as illustrated in Figure 6.

In thermally limited applications, capacitor dissipation factors should be specified for the temperatures and frequencies of interest to facilitate prediction of performance.

Polycarbonate/foil capacitors exhibit small dissipation factors over the temperature range from - 55°C to + 85°C and up to 50 kilocycles.

Size and weight limitations for capacitor ratings of 10 microfarads or larger may be imposed by heat generation and transfer in some applications. Metallized polycarbonate capacitors, that exhibit smaller dissipation factors than metallized paper, may offer appreciable size and weight advantages in the voltage range of 200 to 250 volts RMS for the following reasons:

- 1) Polycarbonate film has a higher dielectric strength and therefore requires less thickness and volume than paper.
- 2) Polycarbonate film has a smaller dissipation factor than paper and more capacitance may be packaged in a container to achieve the same heat generation as paper.

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The Bendix Corporation Bendix Systems Division Ann Arbor, Michigan Attn: K. A. More (1) The Bendix Corporation Red Bank Division 1900 Hulman Building Dayton, Chio Attn: R. N. Earnshaw (1)

VARO, Incorporated 2201 Walnut Street Garland, Texas Attn: J. H. Jordan (1)

Aerospace Corporation
P. O. Box 95085
Los Angeles 45, California
Attn: Library Technical Documents Group (1)

Engineered Magnetics Division Gulton Industries, Incorporated 13041 Cerise Avenue Hawthorne, California Attn: Burton J. McComb (1)

AiResearch Mfg. Co. Div. of the Garrett Co. P. O. 5217 Phoenix, Arizona 85010 Attn: Mrs. J. F. Mackenzie, Librarian (1)

General Dynamics Astronautics Dept. 963-2 5001 Kearney Villa Rd. San Diego, California Attn: R. Schaelchlin (1)

Prestclite Toledo, Ohio Attn: J. F. Carey (1)

Director of Research Lab for the Engr. Science Thornton Hall University of Virginia Charlottesville, Virginia Attn: A. R. Kuhlthau (1)

Radiation Effects Information Center Battelle Memorial Institute 505 King Ave. Columbus, Ohio 43201 Attn: E. N. Wyler (1)

APPENDIX A

Capacitance and Dissipation Factor Test Data

Data contained in Tables Al through A6 were obtained by bridge measurement and calorimeter data with simusoidal voltage waveforms.

An example of the dissipation factor corrections applied to the bridge data is given here:

From Table Al, capacitor No. 1A, the dissipation factor as determined from the bridge data at 10 kilocycles is 1.110%. As measured by the calorimeter, the dissipation factor at 10 kilocycles is .975%.

By ratio of the bridge data of the dissipation factor for capacitor number 1B and 1A, the corrected dissipation factor for capacitor 1B at 10 kilocycles is:

Test data for capacitor numbers 2E, 2B, 3A through 3E in Table Al were not included in the plotted results in Figure A2. The reader is referred to page 3 for reasons of omission.

Test data for capacitor numbers 2E and 3D in Table A4 were not included in the plotted results in Figure A8. Also test data for capacitor numbers 10A in Table A5 and 8A in Table A6 were not included in the plotted results in Figures A10 and A12 respectively. The reader is referred to pages 4 and 5 of this report for reasons of omission.

25°C TEST DATA FOR METALLIZED POLYCARBOWATE CAPACITORS

			CAMCITOR		- L	2 4	400 VDC	•			2 MFD	400 VDC					2.5 MFD	400 VDC					2 MFD		400405				2MFD	300 VDC		
		5	////		200	258	395	1.020		790	.200	136	818.			5	28	1.215	7	1.292		703	75	23	723	ŭ	7	1/2 60	7	169	7	ð
GE				 ' -	343			+			_		-	_		7 1.240	2,060 3.980	2.1 5		-			4 .675	7 .703		3 .693	1	2 907		\dashv	1351	3 .860
BRIDGE	3	2		'	ļ	ŀ	_	<u> </u>		818,	482	<u> </u>		1	/	5777	-		1	. 613	///	.280	272	.277		. 283	///	358		1332	.380	£
TED	36	m			85/	<u> </u>	1	 -	-	209		-:	<u> </u>	,		.363	(.300	,233	1	98€.		161	787	1.89		197		.238	161:	722.	.254	.231
CORRECTED	HA	_		,	.132	138	. 48	151.		,124	. 154	38	124	,		./78		./83	١	981.		134	132	./36	134	132		139	121	135	141.	.136
00		4.		ı	8	27	. 13/	.134		.095	001.	760	.092	1		166	225	79/		162		8	560	20%	.995	560		860.	.093	660.	850.	660
		777	777	1	Z	Z	7	Z	Z	Z	7	Z	Z	Z	7	7	Z	7	Ž	Z	Z	Z	7	\mathbb{Z}	Z	7	Z	Z	\overline{Z}	Z_{ℓ}	7	Z
47		.5		279.	ı	1	1	1		,	1	1	1	1.570		1	,	1	£ 76	,		•	,	1	1	•		,	,	1	1	•
FROM ER DATA		4		.400	1	ı		,			١	ı	i	.610			ı	1	1.750				•	1	1			;		•		•
D FR TER	DF (%)	'n		177	,	١	1	,		,	ı	1	i	.390		1	ı	1	1.070	,		,	1		1			,		1	ı	<u> </u>
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CALCU		4		./42	1	,	1	1	1	1		J	,	104		,		•	2.10	•		,	1	,	,			1	,	1		-
		1/1	////	1	/		/		J	/	1	/	/	/	1		7	7	1	Z	7	7	7	7	7	7		7	7	7	7	7
		0/		1.110	958	179.	1.020	1.160		1.650	2,500	2.040	1.710	3.280		1.810	5.830	1.770	5.470	1.890		1.470	1.410	1.470	1.510	.450		1.8%	1.380	.350	.980	1.790
		h		.581	507	525		419.		844	1.280		.874	1.620		406	3.250	.893	2.750	596		744		.736	-1	753 /	\sim	.943			1.010.	.9/3
NTS	\mathcal{Z}	3		.408		_1	379	824	3	537	.797 1.		. 858	1 000.		595	£ 040	.369	680 2	1007	J	490	479	484	502	492	\sim	. //3	404	\rightarrow	1 050	ᆜ
EMEA	DF			361	316		.353	361]	3	430	. 387	% %	499 1.		.340	,837 2.	+	.708 /.	354		336	,332 4		337	332		390	388	379	.395 .	381
MEASUREME,		4.		.731	-		.676 .3	690 .3		529 .3	555 .4	_	509	579.4		.503	8, 282.	503.	- †	489		525		590 .3	530	530 3		544	.519	_1	547 .3	\dashv
ME		.v.	1777		7.57	.660	ور	2		/s	\range is	Zi Vi	,	Z s		\sigma	10	\ \(\dols\)	769.	4		// ?	3	ZZ V	Z,	5		S	5	7	7	1.55
BRIDGE		0		165.	7866.	.010.	.975	.952		2.238	2.238	2.211	.263	2.197/		2.763	2.703	2118	739	2.731		1.97	1.992	1.367	2001	2,040/		Z.017	2.003	1.958	2.060	2.004
M BR		5		984	986	1.000.1	.969	.967	3	2,206 2	2,207 2	2.194 2	22 22	2,166 2		2.712	2.690 2	2.668 2.718	2.700 2.739	2.681 2	7	1.947	_	1.941	1.974 2	2.012 3		. 166		7.938		PL6.1
FROM	(MFb)	m		683	986	-	.967	. 996	7	2.198 2	2,201 2	2.187 2.	2.22 2.24 2.263	2,159 2		2.703 2.	- 1		\rightarrow	2.671 2	7	_+	-1	_7	1.968	2.006 2	\leftarrow	1.986.1		1.927 /		1.970 1
CALCULATED	<u>ئ</u>			. 980			.965	. 696.	7	2,192.2.	95 2	912.	_				2.686 2.689	2.639 2.651 2.658	2.688 2.690	62.2.				~1	- 1				967 19	-1		1.965 1.
רכתרי						-+			$\overline{}$			181.20	3 2.216	10 2.153		13 2.688	8 2.6	9 5 6		19 2.662	3				19 1.963	50 2.002		10 1.981			1	
5		4.	0.1	.965	.970	186.	.95	.956	3	2.179	2,183	2.170	2.703	2.140		2.683	2.668	2.63	2.672	2.649		1.920	1.945	1.916	1.949	1.95		1.970	1.956	1.910	2.008	1.953
		FREQUENCY (KC)	CAPACITOR NO.	4	9	ပ္ .	4	m m		24	78	20	20	26		&	M)	ر س	30	m m		S. A.	56	ე გ	25	SE		S	മ '	၂ 9	વુ	2

TABLE AI

25°C TEST DATA FOR POLYCARBONATE/FOIL CAPACITORS

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				777					1117										-		
95%	\vdash	858' 258'	8.864	\mathbb{Z}	719	310	. 46.	.422	763	-	1			,		7. 80/	0. 950.	1. 480'	2, 40%	234	
.852	52 .855	25 ,856	198. 9	Z	\vdash		1	401	.763	Lar.	250. 1	580	/0/	2,3	Z	1	•	i		7	- MFD
858.	58 .860		198. 10	Z	.708	338	.303	214	174	7		1	1	ı	7	0, 901.	0. 190.	1. 980.	7. 901.	1237	400 VDC
958	-	-	Ľ	\overline{Z}	.695	323	4	-	774	'	1	,	ı	1	Z	104.0	0. 850	1. 480.	164 .2	237	· V
00			798. 0	Z	.692	316	من	4/2	773	-	•	•		•	Z	104	0: 150	1. 580.	401.	236	
N		7		1	\sim	71		$\overline{}$		1	\searrow	ブナ	1		1	1	1	1		7	
6.	1.910 1.985	\neg	1991 2.019	Z	. 503 .	337	. 523	/ 128.	1.660	150'	7 .055	9	140	37	7	•		,		7	V
1.9	.972 1.984 1.990		1.995 2.024	\overline{Z}	499	. 330	.526	.921 1.	1.690	'	ı		1	1	Z	056	. 655	911.	. 40	730	2 MFD
786.1 865	1661 98		1.997 2.025	7		327	, 519	1813	1.650	-	,	3	,	1	7	.056 .	_]	1.511	1.38	7351	200 1/00
1.985	-	1.991 1.997	17 2.024	Z		.332		-	70197	7	١.	1	,	,	7	2. 720.	. 250.	116	40	122	\ \ \
6.	-	. -	1.992 2.020	/	-	_		\vdash	.650	7	,	,	,	'	7	. 057 .	. 054	115	39	1322	
	1			7		1	1								7						
w.	3.108 3.1	3.117 3.131	31 3,200		.480	7%	1 349.	1.110 2	2.310	1.050	7 .038	2.	107	70%	Ż		1	,	1	-	•
w		_			\vdash			1.250 2	2.590	- 7	1	,	1	1	Z	. 550.	.040	.073 .1	6. 411.	122	3 MFD
2.950 2		2.972 2.985	85 3.048		_			-	2,260	1	ı	١	,	1	7	. 450.	.038	. 065	1. 00 /	861	135 VAC
		3.107 3.121	21 3.193	Ž	265				2,420	-	1	'	1	3	7		, 980.	1. 070.	2' 80/	212	
	3.018 3.6	3,028 3.043		Ž	l	_	'		2.40	1	i	١	1	,	7	,054	. 039 .0		. 106	210	
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TABLE A2

25°C TEST DATA FOR METALLIZED PAPER CAPACITORS

			CAPACITOR RATING		2 MFD	200VDC	24007				7 457	Z	400 UC				2 AFD	400 VDC		.,					·							
		111	177	4		N		4	7	1	7		7	7	11	Z		/			4						1		7	∇	V	4
		6		1.115	1.205	.545	1,090	1.127		1	.960	925	1 095'	355		1.305	200	861.	1.215	305.											7	7
BRIDGE		5		3		, 596	.457			1	.378	372	378	384		462	.462	1462	L		1				-						1	-
1	DF (%)	M		3	Ш		431	438	3	-	345	341	345	.351	1	.417				-	\sim										+	_
CORRECTED	PF	-		22		,266				1	.188	186	-			most.	1 1	121	3												\dashv	\dashv
CORRI		4:		351	-	351	338	7768	7		1. 11.2.	272 .1		275 .1		302	-		,											1	\dashv	\dashv
1		177	111	//		7			X	7	4	7	1	7	1		4		:		/	-				_	1	7		4		4
		777	///	1					J	7	77	77	7	7,	1	30	10/	7	20	8	7					77	1	7		7	7	7
EOM		,		<u> </u>	,	•	١	•	7	955	-	'	١	1		0 2.730	0 2,710	0 2,700		0 2.730										4	1	4
12	3	\ <u>\</u>		<u>'</u>	1	1	•	-		1.386	'	•	1	-		0 1.640	0 1.630	01.620	097.10	0281 0										4	\dashv	_
CALCULATED CALOKIMETER	J A	m		1	,	ı		,		.35	•	ì	١	•		1.250	1.220	1.740			/]							\downarrow	_
CALCULATED CALORIMETE				'		1	•	•		261. 3	<u>'</u>	•	_	٠		80%. 0	998.	\$16.0		759. 0									-	\dashv		4
33		4.		,	·	,	,	•	7	1275	'	,	'	-		1.010	1.000	010.1	1.010	1.050			Z		7					4	_	4
		777	7777	20	30	9	3	3	7	3	2	30/	2	90	1	30	9	00	Sol	8			7	7		7	7		7	\rightarrow	4	4
3		0 /		2.520		0 3,490	20 2,460	50 2.550	7	2.160	40 2.170	0 2.090		09/.2 00		10 2,730		0 2.700	0 2.750	2.730										\dashv	_	4
RE MENT	<u>જ</u>	2	<u> </u>	5 1.630		.570 2.110	290 1.620	310 1.650	7	.050 1.370	,030 1.340	1.020 1.320	i	6 1.360		0 1.640	220 1.630	240 1.620	0 1.660	0.820											+	4
	DF (. 60		0 1.325	-	_	-		7	K	\preceq		0501/	1.050		8 1.250	\rightarrow		8 1.250	7 1.270									_	\dashv	_	4
MEASU		1		0 1.030	0 1.030	0 /./ 00	0/0//	0/0//	+	-+	5 .776		787.	.788		806. 0	668' 0	416. 0	805. 0	137										\downarrow	_	_
BRIDGE		4	,,,,	1.170	1.320	1.170	1.130	1.120		1917	305.	906	216	1917		1.010	1.000	1.020	1.010	1.050		X.		7	7	7				4	7	
BR		7777	1111	5	7		3	5	7	4	7	7	2	5		217	3	7 26	S	S	/	7	7	~		~		4	7	7	7	4
FROM	ζ,	0/		9 1.855	L981 b	1351 5651	988.7	0 1.877			9.875	\rightarrow	-7	688.7		~		10 2.199	8 2.215	167 2.95									_	\dashv	\rightarrow	4
	Fb)	40		658.	8 1.849		898.7 2	9 1.860	v	178.10	3 1.856	7.869	8 1.859	7.87/		3 2,184		9 21.70	7	4										\dashv	\dashv	_
CALCULATED] (MFD)	n		3 /.835	848.1			1 1.859	\mathcal{A}	- 1		1.866	٦	898./ 0		2,178		1 2.169	9 2.186	7 2.164								_	_	_	\dashv	_
7777)			/ 843	1.850	1.939	_ 1	7.87	$_{L}$		7.856	\supseteq	7.860	1.870		2.181		12.171	2.189	2.167											\perp	
3		4.		7.838	1.847	1.933	598.7	1.859	1	1.863	7.848	1.858	1.852	1.867		2,175	2.160	2,164	2.183	2.161												
		FREQUENCY (KC)	CAPACITOR NO.	4	94	7	4	4		<u> </u>	9	2	5,	76		~	9	<u>ي</u>	Q	8¢											-	

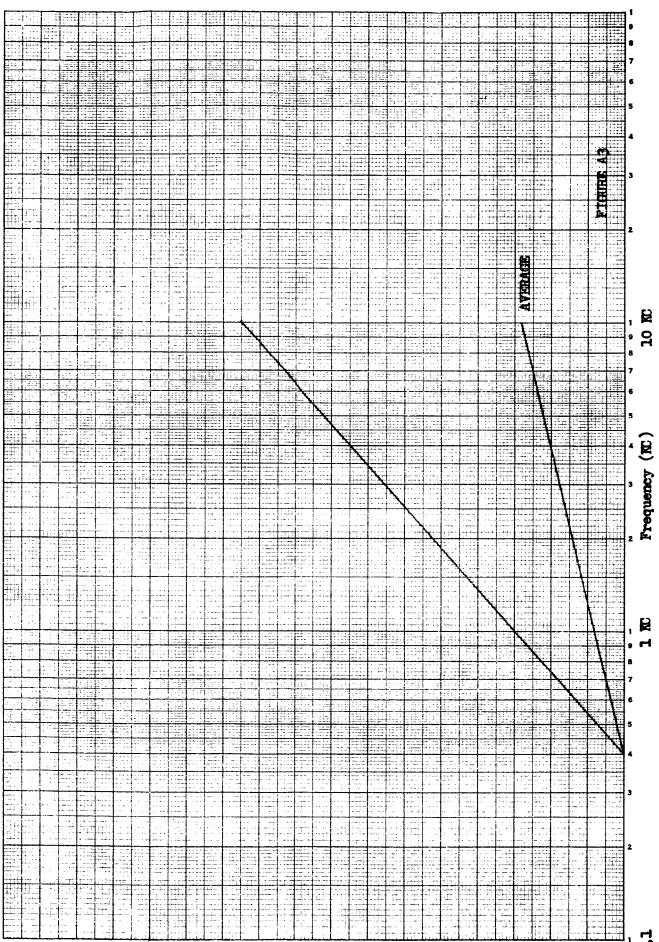
TABLE A3

3 eye. x 170 1mm Divisions

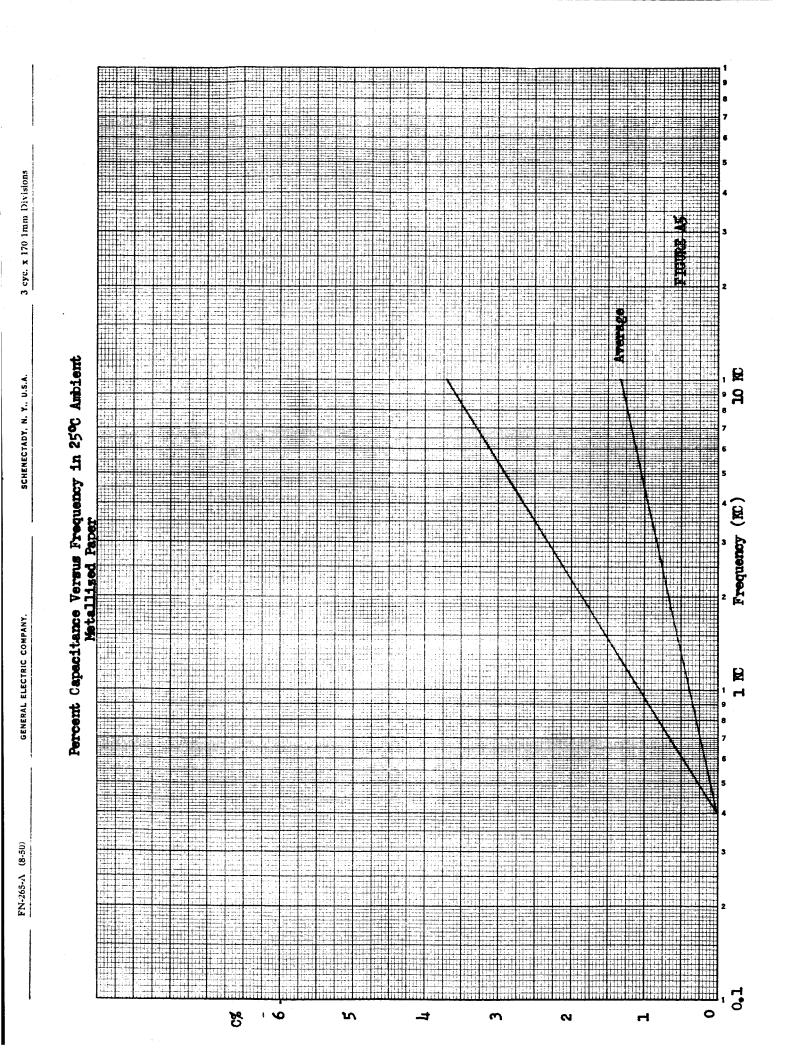
SCHENECTADY, N. Y., U.S.A.

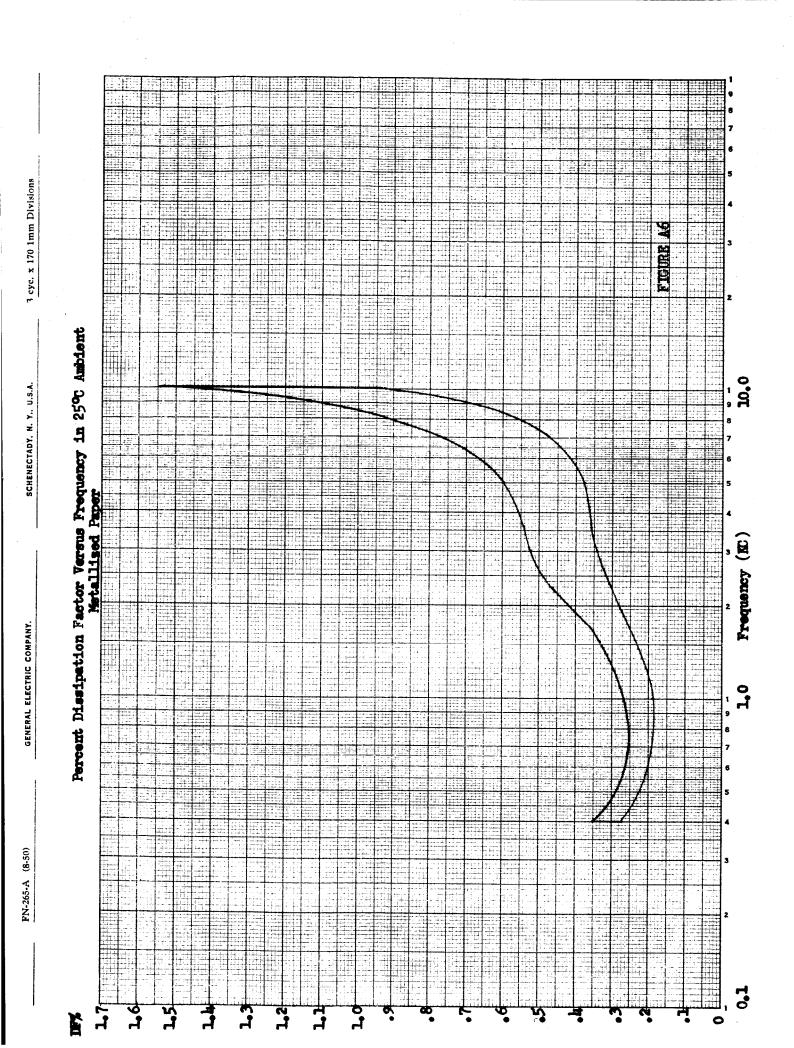
GENERAL ELECTRIC COMPANY.

FN-265-A (8-50)



N





CAPACITOR TEST LATA VERSUS TEMPERATURE
FOR METALLIZED POLYCARBONATE CAPACITORS

			AMBIENT TEMPERATURE		0	1920			777777		. 26.	ナイじつ					٦٢٥	ンヘアー		11111111	7777777			J.25-			7777777					
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		0/		1.025	1.800	M)	1	.739	7	\perp	015.1	3.7		699		+	1.895	3.606		95		1.120	6.300	m	_1						\downarrow	
L E		2		407	702	1.850	.290	.355		8	919	370 1.070 1.750 3.740	.283	332		.523	757.	.710	312	5	3	.513	2,510	1,630	351	402						
38	જ			177	447		25	378	, Y		30	702	192	777	1	294	495	-	27.7	259	7	314	1610 2		797	290				+	\dagger	+
43	DF (%	M		_1			-1	_	1	1		21.0			$\langle \rangle$		-	-+	-1	_	$\frac{1}{2}$	-1	-7	\rightarrow	_1	_	X		_	\dashv	+	-
PEC7		-		140	194	384	.128	148			- 1	.37	/32	. 135		179	7	408	175	-2		220	8/9	414	412	./90						
CORRECTED BRIDGE		4:		132	801	502	750	160	1	147	4	210	260	560	7	#	7	245	8//	3		17.	253	197	135	¥						
		///		1	j	7	Z	1	X	7	1	7	7	4	7	7	7	Z	7	Z	7	Z	Z	\overline{Z}	\overline{A}	\overline{Z}	\mathcal{X}	Z	\overline{Z}	\overline{Z}	\overline{Z}	7
		0		2.000	7.610	9,650	3.030	3,300	7	700	6.630	9.140	2.390	2.980		2.390	90.8	.800	3.18	3,110		2.180	13.080 26.610	3.420	1.840 3.25	3.360						
					1	-		-	\leftarrow	+				1.480 2	7	1.290 2	3.940 8	4,460 8.800		1.650 3	7	1.260 2	2080	3	40	79.0	Z			\dashv	+	\dashv
	(5		/000	3.660	4.830	1.520	ر. وي	1	28	3,180	4.570	7.480	_			3.9				7		13.0	4	81/6		7			\vdash	\dashv	4
478	%)	, m		.657	2.210	2.920	516	96		1659	930	2.780	,912,	.961		.873	245	2.780	1.080	1.10	N	538	3,010 7.980	2.680	0127	1.230					İ	
MEASUREMENTS	DF			449	.87%	0717	456	470	7	485	804 1.9	080.	471	,490		.574	1.030		626	638		708	0/0	2012	.763	£8						
SURI	7						- 1	Т	\mathcal{L}	1	_1		574		7	ĺ	815 /.	930 1.190	709	\dashv		_	3	7/ 0		908	/	-		\vdash	\dashv	\dashv
MEA		4.		889	724	.792	554	28		. 43	,694	, 79g	5	,50		.758	<u>∞</u>	6	7.	72.1		.88	1.690	96'	8/8	3					_	
1 1			7777	\mathbb{Z}_8	1	2	3	7	7	1	Ž	75	727	183	X) 	7	7	2	8	1	7	w 7	3773	\$ \\	7		7	7	1	7	4
Ä		0/		1.008	2.248	2.72	2.083	1.99.7	1	7.6	2.233	2.773	2.076			900	2.158 2.216	2.698 2.778		1.970		.980	2.193				∇					
BR	1	5		.993	2.187	2.657	2.010	1.947	7	787	2.157 2.174	101.	2,020	1.938		.877	5	859	100.5 4921	1,924		695	2.139	2.662 2,678	1.987	1.908						
POM				\vdash					N.	385	512	84 2	09 2		7	375	18 2	(3 2	14 2	1.3151		975		_	162	1 0061	~	-	-	$ \cdot $	\dashv	ㅓ
A	C (MFD)	80		.990	21.15	2.641	2.004	1.937	\prec	-	2.1	2.6	2.0	1.929			2,16	7.6	1.50				2	2.6	1.979	_	₽,	_	_	Ц		_
ATE	0	1		.987	2.166	2.632	2.007	.93		1	.152	6.74	200.	1.922		696:	.142	678	990	1912		365	7.127	2.659	1.975	768						
CALCULATED FROM BRIDGE				975	_			890 /	V	365	2,140 2,152	2.662 2.674 2.684 2.701	.989 2.002 2.009	1316		796.	2.148 2.142 2.148	2.671 2.678 2.683	.979 1.990	106		156	Ī			1887	77	+		\prod	+	\dashv
162		4.		6,	2,155	2.617	1.989	8.7	7	2	ā	2.6	6,	6:1		6.	2.1	2.6	6.1	1.9		6.	2.1	3	1.9	8.	1					
		FREQUENCY (KC)	CAPACITOR No.	41	2E	35	5 F	ر و		€	2E	35	56	Ų W		₹	2E	প্ল	SE	90	•	۷	2 E	3D	SE	7) >					

TABLE A 4

CAPACITOR TESI DATA VERSUS TEMPERATURE FOR POLYCARBONATE/FOIL CAPACITORS

		AMSIENT TEMPERATURE			2030) (7+			_		1 + 85°C					-	-15°C	•		7//////	× 10	1	しつねなー			7//////			<u></u>		7
		7777	7777	77	7	7	4		71	7	7	4	7	11	7	7	1	7	7	17	4	1	4	4	4	4	7	4	4	\mathcal{X}	7
		6																						1			1	+		1	
		2				_		11			_	_									-		+	-			+	+		+	
		8					_					_							_				-	_			-	\downarrow	\downarrow	_	
		^						1111								_	-		_			_	1				-	\downarrow	\downarrow	-	
		4														4								1			1			1	
	}	7777	7777	\overline{Z}	1	4	7	1	7	7	7	7	77	X	7	7	7	4	7	74	7	1	\	+	4	\mathcal{A}	7	4	7	42	4
ıμ'	1	8		4 52.	.226	.202			,210		. 197				,251	- +	.192	_				1.352	.200				_	_	-	-	4
BRIDGE	0	Ŋ		401.	3	701.			101	132	380		_		611.		.097				4	.853	.10	_	_			1	_	_	_
ł .	DF (%)	w		-084		.08			ררס.	80/	.063				880		890.	_			.137		\$70.	-	_		-	_			
CORRECTED	, ,	`		950.	.055	850.			83	.050	.035				.075	. 693	.043				8	- 276	.050	_			-	_	_	_	_
Cox		4		1.08	750.	250'			701	450.	.053				1.124	1.076	190.				.146	791.	40.	1				4	4		
		7777	777	7	Ž	77	7	1	\overline{Z}	\tilde{Z}	Ž	//	7	4	$\frac{2}{3}$	7	6	77	7	7	\mathcal{L}	7	7	7	4	X	77	4	4	4	\vdash
		0		1.420	4,640	5.260	-		1.280	2,1504.360	5.110				1.520	7.500	2.390 4.990				0897	27.700	2.630 5.190				-		_	_	
MENTS	જ	b		747	2.270	2,460			707.				_		959.	٠. گ					823 1.040	350 13.820 27.700							_	\perp	
REME	公片	พ		.505	/.380	/,480			465	-	589 1.380				\$25.	1.020 2.330	1.500				1	8.350	1.700								4
MEASURE		_		.404.	129.	.1 259.			,384						.539		_				.694	1.750 3.130 8	.837								
1		4		કુ	819.	.587			.683	.594	. 595				194	,827	.683				7.934	1.750	.88.								
3		7777	777,	1	\mathbb{Z}	\square	27	1	\angle	7		∇		7	\downarrow	\angle	\sum_{i}	/	7	\searrow	\overline{Z}	7	Ż	77	7	4	7	7	7	77	4
BRIDGE		0/		698.	2.046	3,305			.874	~	3.124 3.269				.862	7	3.293				.954	1.966 2.011	3.136 3.282								
1	(A)	٦,		858	2.000	3.150			. 865		<u>v</u>				.855	1.985	3.147				.847										
D R	C (MFb)	3		.857					198	1.997	3.092				458.		3.105 3.120 3.147 3.293				748	1.959	3.109								
CALCULATED FROM	U	,		854	979.	r-r	1		958.	1.990					158	1					288.	6561 6561 6461	3,089 3.097 3,109								
CALC		4.		843	_	3,089			.847	1.976	3.058				8. 9.		-				.835	1.947	3,089		,,,,,,						
		FREQUENCY (KC)	CAPACITOR No.	9.8	₩0/				44	40/	1				46	40/	4/		-		96	40/	4/								

TABLE A5

COLDS TEST THEN VICES TEMPS AND NE FOR METALLIZES FOLER CORDS SOLE

	3	~	() A	8	الم الم		7:0KG	15 N				3 y.y c 2	CORRECTED	5	w l			*		
-	Ì	U	(MFD)	ļ.	Ì		'	L A	(%)				DF(X)							
	4	`	u.)	l _n	6	<i>1111</i> 4:		w	in	9	111 2:		m	h	0			 		
CAMC.TOR No.						1771	•				///								AMBIENT TEMPERATURE	The S
	7.865	1.874	1.867	7.86	1.932	8.	818. 278.	3 1.380	2.040 3.850	3.850	1.256	421. 0	1 .356	399	1.060				7	
ت	1.909	1.919	1.922	1.930	1.982	6.	.986 .872	j		3.800	1.276	811. 9	1321	.366	136.			•		
		2,045	2.050		2.113	8.		-		5.150	1226	651. 9.		1	1.055	7) 4× + Z	.)
						7					7			_		7			Z	
						1					1								111111	
	1,838	1841	8.8	.83.	7.887	1	1.700	201	· I	2.3504.050	351	248	8	9	1115		77777			1
	1.860		1.848		0761	6.	L	-		3.810	275.		Ш		1				, Z	
	21.15		2,183		2.246	7	\Box			5.880	35.	301 108			-	Z			7 + 25 2	٠,
				•					$\overline{}$		Z	\vdash	\Box			Z			Z	
						7		_			/					7			7	
¥¥		1																		7
	1.72	541	1.775	1.776	1087	7	1.630 1.710	N	A60 3,180 4.900	4.900	4.	476 362	289.	549'	1.348	7			Z	
	1.824	248.1	1.825	7.825	7.859	7	1.420 1.43	1.430 2.030		2.630 4.200	\ \ \	398 .293			.482 1.070	7			Z	
	2,014	2.016	2,100		2,138	11:	1.710 2,140	~	5.500	5.500 9.560	4	457 392	856. 7	8.	1.960				Z - 25°C	
				1 1		Z					7					7			Z	
						7				,	7					7			Z	
لحب																				/
	1.721	1.915	1.692	689.7	1.704	1	2.330 2.500	m	3.550	5,230	189.	.530	0 ,847	477. I	1.940	7			Z	
	1.775	1.773	1.762	1.761	797	//	1.810 1.85	1.850 2.390 2.960 4.700	2,960	4.700	7	509 .378	8 563	i	542 1.175	7			Z	
	2.033	2.02	2.027 1.920	1.980 2.001	7.001	3.5	3,400 5,11	5,110 10.470 15,460 28,260	15.460	28.260	016.	938		2,040 2,23 5,795	5.195	7			7 - 55 0	`
						7					7		_			7			7	
						//					7					Z			7	
			////																	1
						7							-			7		-	Z	 -
					,	7					7					7		-	Z	
						7					7					7			Z	
						7					7					7			\overline{A}	
						7		_			7					Z				

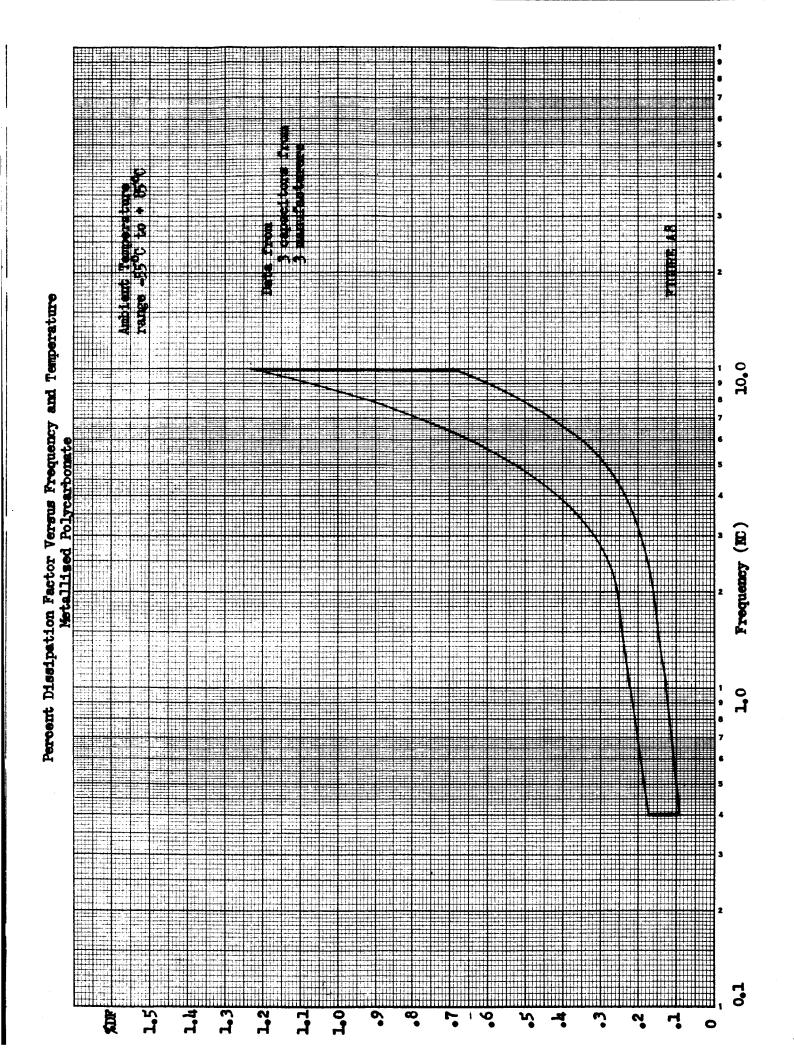
TABLE A6

Q

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Auch and Temperature range -55°C to +85°C Percent Capacitance Versus Frequency and Temperature Polycarbonste/Feil Frequency (EC

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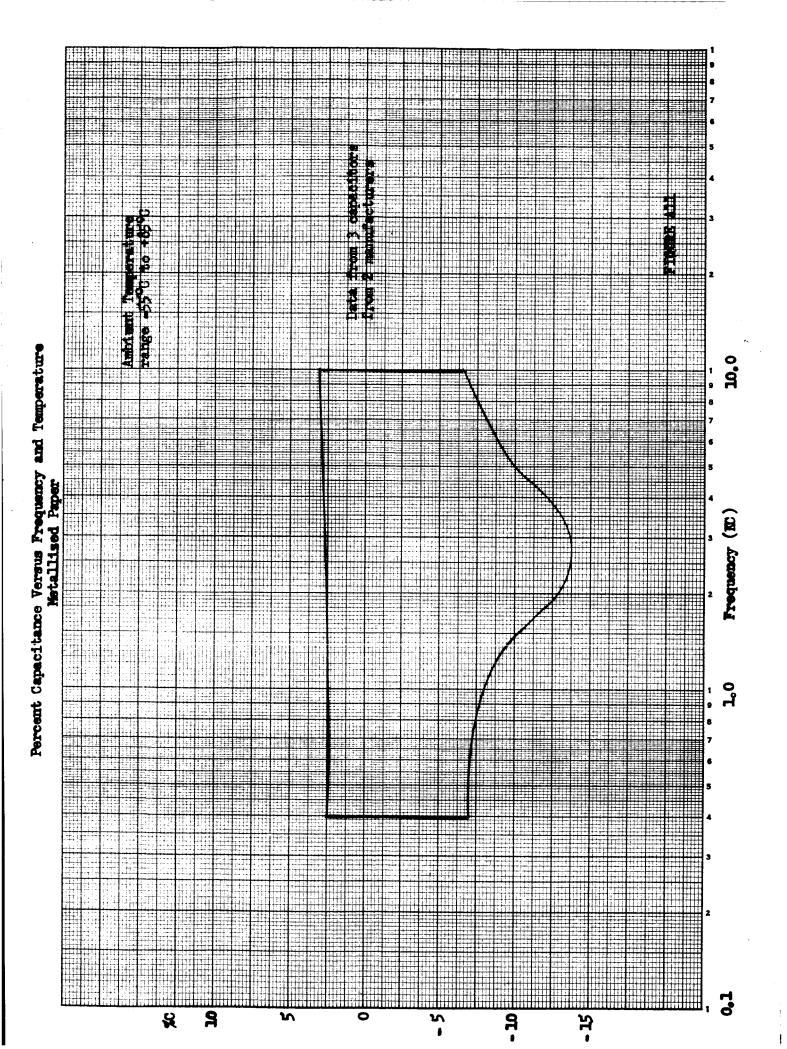
7

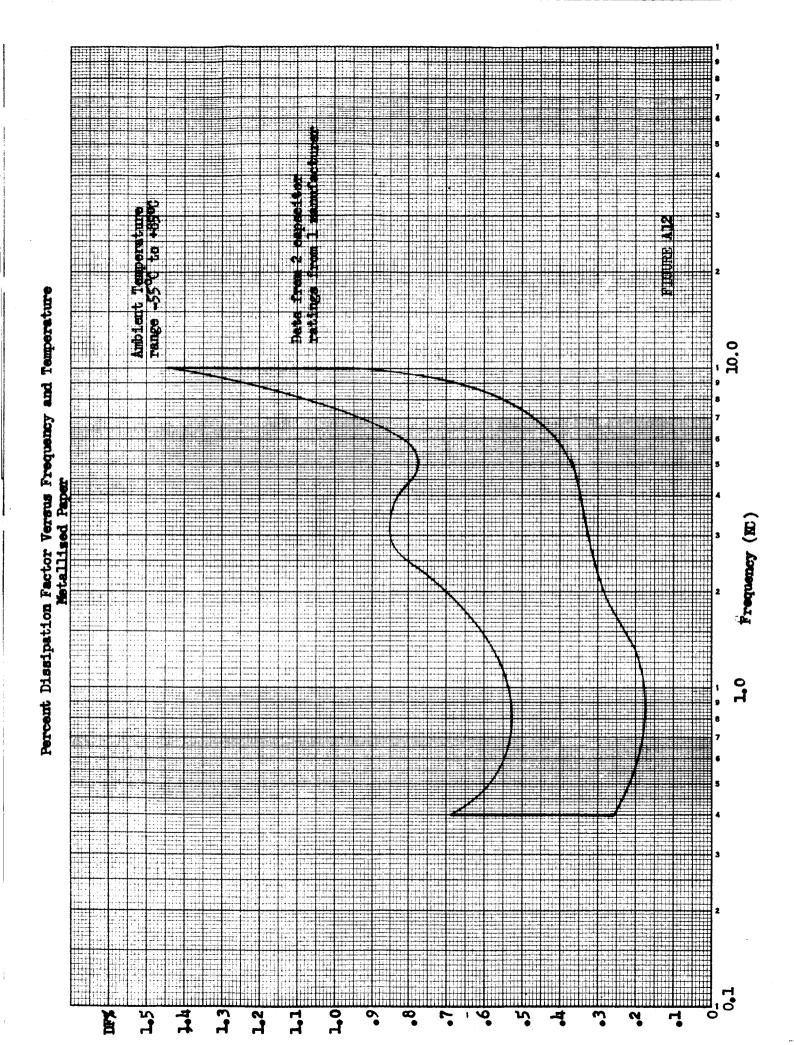
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4 cyc. x 170 1mm Divisions Patenta Min Percent Dissipation Factor Versus Frequency and Temperature Polycarbonate/Foll Frequency

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APPENDIX B

Capacitance and Dissipation Factor Life Test Data

Test data contained in Table Bl were obtained before and after a 1000 hour life test in 85°C ambient with 400 cps voltage applied.

Capacitors with 400 VDC rating were energized with 325 volts peak. Capacitors with 200 VDC rating were energized with 212 volts peak. The 135 and 157 volt DC capacitor ratings were energized with 162 volts peak.

The 325 volt peak limitation was maintained to prevent damage to the capacitors from corona.

An example of the method of obtaining correction factors for the dissipation factor is given:

Bridge value of dissipation factor for capacitor number 1B before life test is 0.316% and is equivalent to the corrected DF% of 0.132 from Table Al at 1 kilocycle.

Bridge value of dissipation factor for capacitor number 1B after life test is 0.326%. The corrected DF% is obtained by:

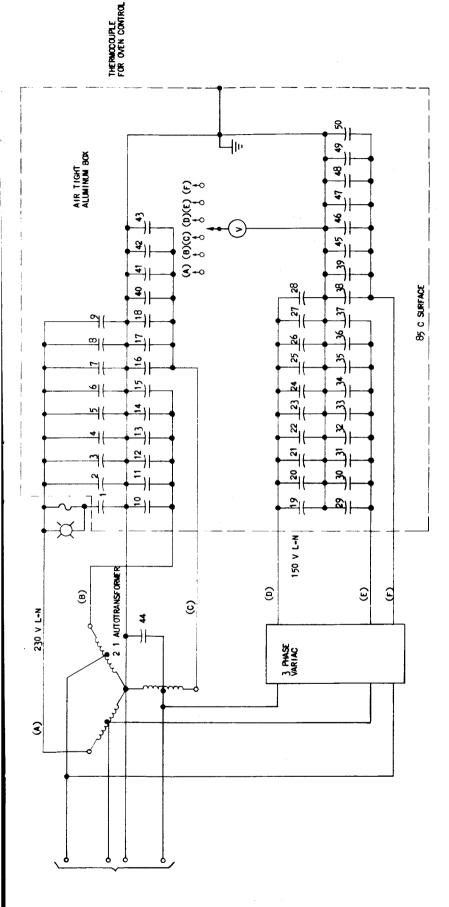
 $\frac{0.326\%}{0.316\%}$ x 0.132 = 0.136%

Vening D. Tout . P.

REFORE ALL AFTER LIFE IE.

₽¥	BEFORE L	LIFE TE	TEST			AF,	AFTER LIF	Y	76.37			BEFC	JAE 1	FE	TEST			AFTER	FR LIFE	FE TEST	7		
	BRIDGE MARS	١.	Series.		111				للمعجعي	777	~		PRIBGE MEAS.		نَّهُن	777	(11)	هم ا	FRITGE MERE.	يحلنانيوي			
CAP.	(MF2)	12 S	(%)	CAP.	111	No.	C C Z	100	48	177	2.00	3	(MFB) (%)	A S	LAS.	777	8.00		C DF	14 83 14 83		777	
40	484		+	APC	1				-	77.	156	_	1	803	2	262	156		3,000 428	†	38	7	
آ	.995		./38	MPC		 	+	1		MPC	(O)				9 350	PCF	₹ø/			11 .045	5 PCF		
2	396		148	MPC	/	A	 	•	├	mpe	///	H		365 .0	980.	PCF	7 110		2,962 287		-	7	
Ā	596	.361	151	MPC	/	\vdash	├ ──	├	-	Mec	3					PCF /	2		3.104 .311	1.037		7	
80	2,688	+	۲. 8	MPC	/	-	⊢ —		-	MR	7 : 6			. 379 .O	.039 P	PCF	7 116		3.030 30	160, 10	PCF	\overline{Z}	
				1	1	1	\sim	/	1		1		177						7	/		7	
W.	2.686	354	98/	MPC	/	3E 2	2.680	1322	1691	ME	178	-	5.470 .3	.365	١	PCF 7	178		5.500 4	452 -	ACF	7	
80	1.934	336	<u>;</u>	MPC	/	_			-	MPC	18		3.310 ,4		٥	POF	18.8		3.334 ,4	- 824	PCF	7	
8,8	1.956	337	137	MPC		\vdash			123 1	me	4		1.939 1.		266	MP	40		• ~		-	7	
7	1.931	343	136	MPC		-		.304	121.	MR	4	_	1.871 1.6	6. 010.	744	ON	44	\neg	9. 36.	926. 189.	9 MP	7	
G	1,563	1	.134	MPC		25		80		MPC	4	-	1.864 1.0	1,0/0,	\dashv	MP	14E	\exists	6 648	225. 199	6 MP	7	
							1											7					
S.	7.007	337	./37	MPC	7	5E /	1.995	313	124 /	MPC	7	78 1.8	1.856 .7	1. 277.	88/	NP	78	-+	1.873 .7	281. 021.	\dashv	7	
6.0	1.481	390	139	Mec	7	6A 2	2.003	.401	143 /	MPC	7	70 1.8	2' 8981	.768	186	MP	77	\dashv	7. 885.7	144 180	o Mb	7	
90	-	.379	735/	MPC	Z	ود ا	1.943	. 379	138 /	MPC	7		-	-		_	7	-	-	-	+	7	
99	5951	185.	136	MPC	Z	99	1.983	. Į	137	MPC	J		-	-	-	1	4	+	+	+	-	Z	
37/	3.008	3,56	ı	MPC	Z	12E 3	3.020	352	-	MPC	4		-		-	7	4	_		_		7	
		, ,			\mathcal{Z}	\sim					//		7	7	7	7		7	7	3		1	
134	3.277	456	1	MPC	Z	13.0	3.307	.360	1	3	7	1	-		+		4	-	1	+	-	Z	
138	3.274	437	3	MPC	7	/30	3.309	,356	,	MPC	7	٤	PC-ME	MPC-METALLIZED	(3E)	1	1		+	+		7	
78/	3.194		1	MPC	Z	730	3226	.341	-	MPC				POLYCARBONNIE	16130N	7910	\	-	+	+		1	
(3D			1	MPC	Z	13D	3.260	.348	1	MPE	4	7	FIRE	PCF-BLTCPRBONATE,	30NA2	/3/	1	+	-		-	1	
136		784	1	MR	Z	13€	3.255	347	(MPC	7		-	7	F014			-	-	-		7	
					3						3	3	3	7		7	1	3	7	7	7	7	
14.0	2.783	.377	1	MR	Z	140	2.813	363	1	36	7	Z	4-01	MP-METALLIZED	126	1	4	-	-	+	+	7	
AC		2.370	3	MPC	7	14c		350	,	MPC	4	+	+	PAPER	9	1	4	+	+	+	-	1	
146	e 2.774	447		MPC	Z	146	2,806	427	1	MPC	1	+	-	+	\dagger	1	4	+	+	+	1	7	
150	3.056	402	1	યુદ	7	95/	3.067	367	,	APC.	4	-	+	+	+	1	4	+	+	+	+	7	
Cs/		1802	,	MPC	\mathbb{Z}	as/	3.04]	443	1	MR	4	-	-	-	4	7	7	4	-	-	-	7	

TABLE BI



NOTES 1. EACH CAPACITOR FUSED AS SHOWN BY CAPACITOR 1. LIGHTS AND FUSES OUTSIDE OVEN.

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PCF - POLYDARDONATE FILM AND ALUMINAM FOIL CONSTRUCTION WPC - WETALLIZED POLYDARBOWATE FILM CONSTRUCTION MP - WETALLIZED PAPER CONSTRUCTION

FIGURE B1

